

# 1. HOIST DC Motors Mathematical Model (Ref. HDK)

## 1.1 Motor Data:

Motor Type : CD Kinematic shunt wound DC Motor  
 Frame CD6063  
 Mechanical Power : 375 HP - 280 kW  
 Efficiency : 91 %  
 Voltage : 225 V armature 120 V field  
 Current : 1360 A arm. 30/12.6 A field  
 Speed : 850/2070 rpm

Resistances ( @ 25°C: Cold windings)

Armature = 0.0037 ohm  
 Comm (&Comp.) Fld. = 0.0016 ohm  
 => Ra = 0.0053 ohm (arm. & Comm field coils in series)  
 Shunt Field = 11.1 ohm (two circuits in series) => 5.55 ohm (each circuit)  
 => Rf = 2.775 ohm (field coils in parallel)

Resistances ( @ 128°C: Hot windings) = Resistances ( @ 25°C) x [ 1 + 4.3x10-3/°C x (128°C - 25°C) ]

Armature = 0.0053 ohm  
 Comm (&Comp.) Fld. = 0.0023 ohm  
 => Ra = 0.0076 ohm (arm. & Comm field coils in series)  
 Shunt Field = 16 ohm (two circuits in series) => 8 ohm (each circuit)  
 => Rf = 4 ohm (field coils in parallel)

Inductances (Unsaturated)

Armature Circuit Total = 0.3494 mH  
 => La = 0.3494 mH  
 Shunt Field = 19.1 H (two circuits in series) => 9.55 H (each circuit)  
 => Lf = 4.775 H (field coils in parallel)

Torque Constant, estimated linearized value (calculated at nominal conditions)

$T_{mnom} = P_{mnom} / \omega_{mnom} = 279.75 \times 10^3 \text{ W} / 89.0118 \text{ rad/s} = 3142.842 \text{ N.m}$   
 $K_t = K_v = T_{mnom} / (I_{fnom} \times I_{anom}) = 3142.842 \text{ N.m} / (30 \text{ A} \times 1360 \text{ A}) = 0.07703 \text{ N.m/A}^2$   
 =>  $K_t = K_v = 0.07703 \text{ N.m/A}^2$

Inertias

Jm = 250 lb.ft<sup>2</sup> = 10.54 kg.m<sup>2</sup> (WK2) (motor)  
 Jb = 112.5 lb.ft<sup>2</sup> = 4.741 kg.m<sup>2</sup> (brake)  
 Jmec = 142 lb.ft<sup>2</sup> = 5.984 kg.m<sup>2</sup> (drum, gearbox, etc.)  
 Jl = 8.2504 kg.m<sup>2</sup> (rated load (40LT) + spreader & headblock)  
 Je = 2.132 kg.m<sup>2</sup> (empty spreader & headblock)

## 1.2 Model Parameters:

2 DC Motors - Series Connected

Armature parameters:

La = 2 x 0.3494x10-3 H => La = 0.6988x10-3 H  
 Cold: Ra = 2 x (0.0037 + 0.0016) ohm => Ra = 0.0106 ohm Arm. Time Constant  $\tau_a = L_a/R_a = 65.92 \text{ ms}$   
 Hot: Ra = 2 x (0.0053 + 0.0023) ohm => Ra = 0.0152 ohm Arm. Time Constant  $\tau_a = L_a/R_a = 45.97 \text{ ms}$

Field parameters:

Lf = 2 x 4.775 H => Lf = 9.55 H

Cold:  $R_f = 2 \times 2.775 \text{ ohm} \Rightarrow R_f = 5.55 \text{ ohm}$       Field Time Constant  $\tau_f = L_f/R_f = 1.72 \text{ s}$   
 Hot:  $R_f = 2 \times 4 \text{ ohm} \Rightarrow R_f = 8.00 \text{ ohm}$       Field Time Constant  $\tau_f = L_f/R_f = 1.19 \text{ s}$   
 Torque constant:  
 $K_t = 2 \times 0.07703 \text{ N.m/A}^2 \Rightarrow K_t = 0.15406 \text{ N.m/A}^2$   
 Total Hoist Drive Inertia reflected to motor shaft :  
 @ Empty Spreader  $J_{tote} = 2 \times (J_m + J_b) + J_{mec} + J_e \Rightarrow J_{tote} = 38.678 \text{ kg.m}^2$   
 @ Rated load (40 LT) under Spreader  $J_{totl} = 2 \times (J_m + J_b) + J_{mec} + J_l \Rightarrow J_{totl} = 44.7964 \text{ kg.m}^2$   
 Reducer Gearbox ratio (motor shaft to drum shaft):  
 $r = 24.45 : 1 \Rightarrow r = 24.45 : 1$   
 Load Gravitational Torque reflected to drum shaft:  
 $M_l = 40 \text{ LT} = 40642 \text{ kg}$ ,  $M_s = 10.715 \text{ LT} = 10886.976 \text{ kg}$ ,  $M_h = 3.219 \text{ LT} = 3270.665 \text{ kg}$   
 Empty Spreader  $M_{tot} = M_h + M_s$        $M_{tote} = 14161 \text{ kg}$   
 Rated load (40 LT) under Spreader  $M_{tot} = M_h + M_s + M_l$        $M_{totl} = 54801 \text{ kg}$   
 Empty Spreader :  $T_{le} = (M_{tote}.g)/2 \times D_d/2 \Rightarrow T_{le} = 41661.59 \text{ N.m}$   
 Rated load (40LT) under Spreader :  $T_{ll} = (M_{totl}.g)/2 \times D_d/2 \Rightarrow T_{ll} = 161224.27 \text{ N.m}$   
 Friction coefficient reflected to motor shaft: neglected  $\Rightarrow f_m = 0 \text{ N.m/rad/s}$

### 1.3 Motor Block diagram:

