

Author's Reply to Discussion of A Prediction Technique for Immiscible Processes Using Field Performance Data

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Liu's proposed method of plotting N_p vs. $\ln(N_p/W_p) - N_p/W_p$ to extrapolate cut vs. cumulative production plots is not based on a firm theoretical foundation. The main objective of the proposed method is to make long-range forecasts from very early performance data.

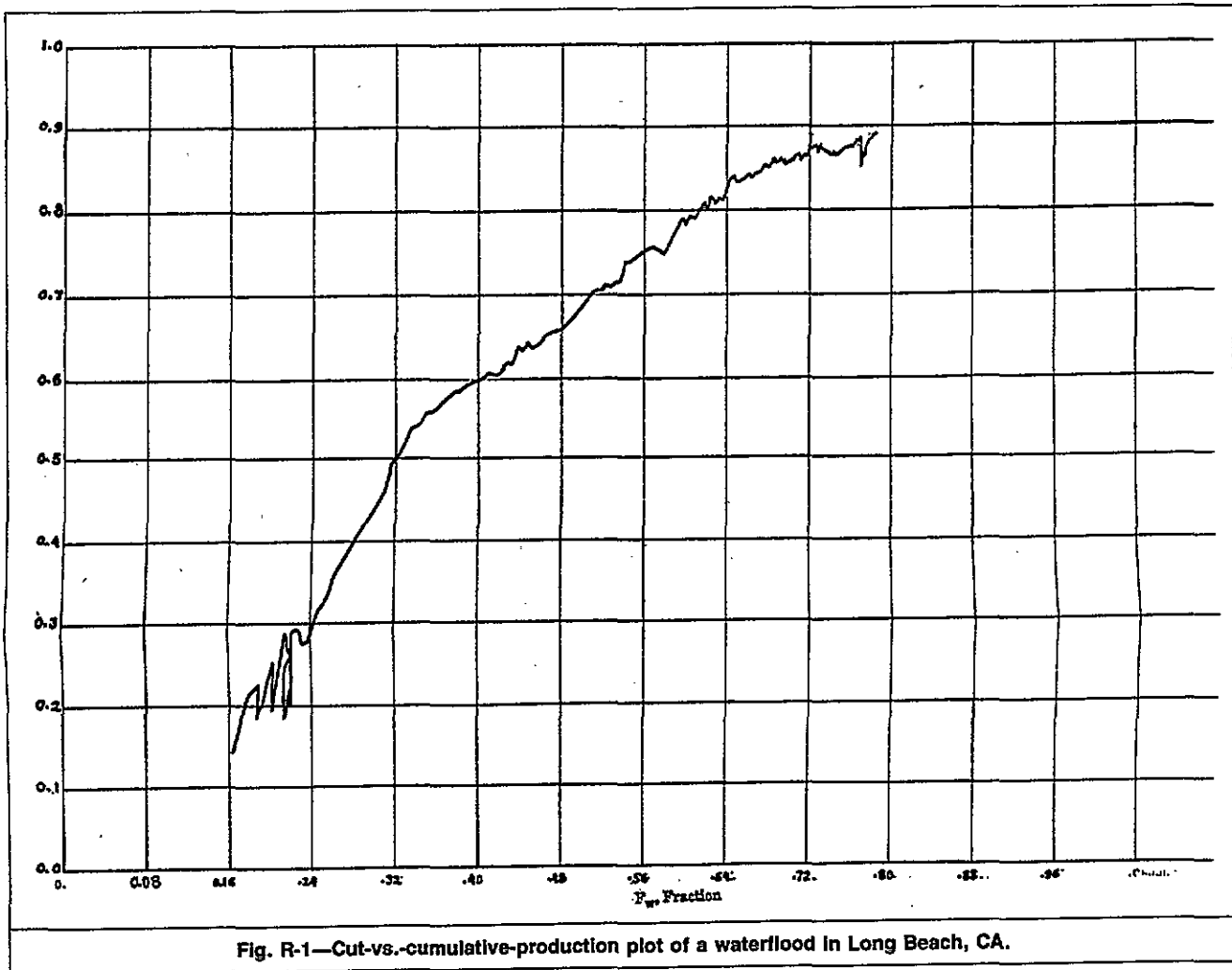
If the prediction technique is to rely on field permeability characteristics of a waterflood, then one must allow sufficient performance data to develop the appropriate trend. Field-based relative permeability characteristics of a waterflood implicitly include a measure of effective vertical and horizontal sweep efficiencies. These efficiencies cannot be reflected unless all producing layers have exhibited breakthrough. Low water cuts (below 50%) are indicative of breakthrough in subcomponents of a layered system. If one believes in the concept of frontal advance theory, then at

breakthrough of all layers, water cut must be above 50% (above the point of inflection of a fractional-flow curve). Thus, applying any procedure to use water-cut data below 50% is to represent the behavior of the reservoir prematurely and can lead to erroneous projections.

The formulation suggested by Liu uses $E_R = mX + n$ as a starting point and substitutes cumulative water cut $F_w = W_p / (N_p + W_p)$ for instantaneous water cut, $f_w = W_p / (W_p - N_p)$. This assumption is not valid because it requires a constant f_w throughout the life history. The relationship between F_w and f_w has a shape similar to that between cumulative recovery and f_w , as shown below:

$$E_R = mX + b,$$

$$N_p = NmX + bN,$$



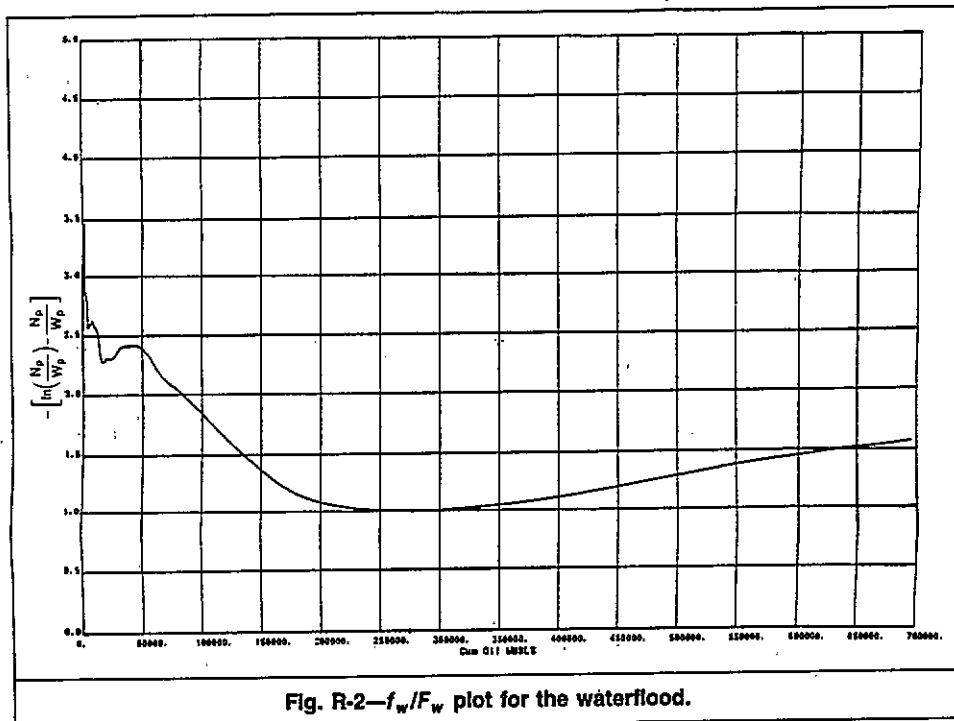


Fig. R-2— f_w/F_w plot for the waterflood.

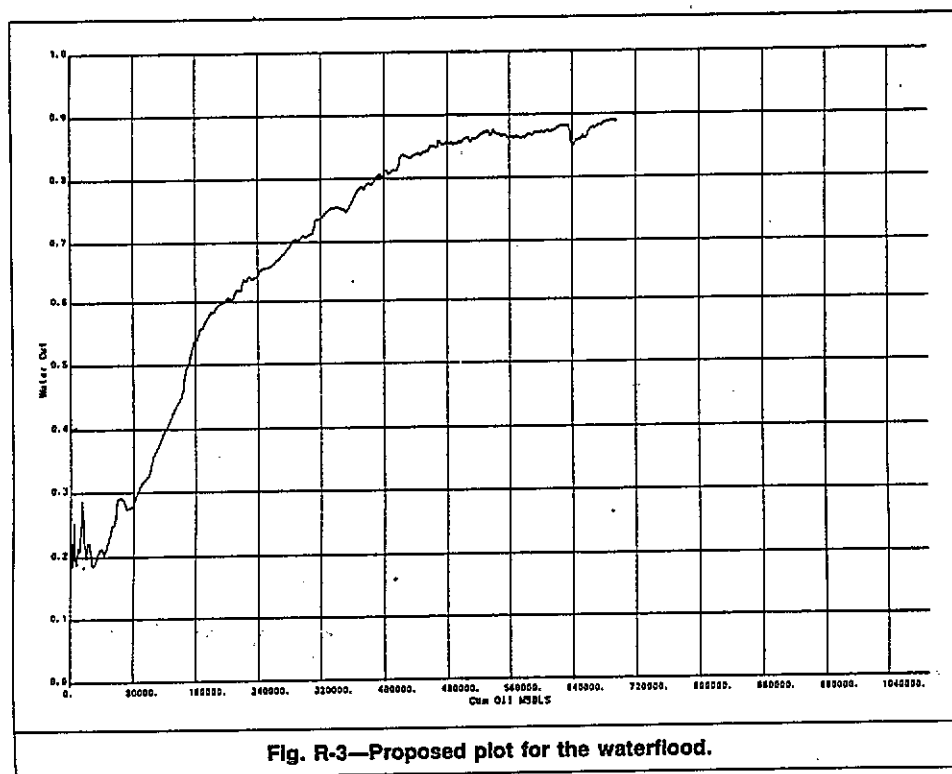


Fig. R-3—Proposed plot for the waterflood.

$F_w = 1 - (N_p/q_i \Delta t)$ (assuming constant injection rate), and

$$F_w = \alpha X + \beta,$$

where $\alpha = -Nm/q_i \Delta t$ and $\beta = -Nb/q_i \Delta t + 1$.

A typical cut-vs.-cumulative-production plot for a mature waterflood is shown in Fig. R-1. Corresponding F_w vs. f_w is plotted in Fig. R-2. Note the nonlinearity of the plot. Also, the plot proposed by Liu is shown in Fig. R-3. There is a definite change in trend starting at cumulative oil production of 32×10^8 bbl [$5.1 \times 10^8 \text{ m}^3$] corresponding to a cumulative cut of 50%. Extrapolation of early

data would definitely have resulted in an erroneous projection. This can also be inferred from a plot of $Z = \ln(N_p/W_p) - (N_p/W_p)$ vs. N_p , where the minimum point corresponding to $dZ/dN_p = 0$ occurs at $N_p = W_p$ or $F_w = 0.5$, which further delays the projection process.

SI Metric Conversion Factor

$$\text{bbl} \times 1.589 873 \quad \text{E-01} = \text{m}^3$$

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