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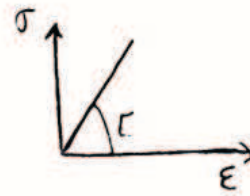
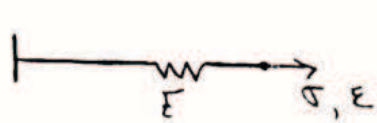
**FACULTAD
DE INGENIERÍA**

“VISCOELASTICIDAD”

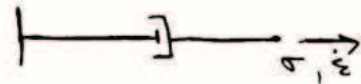
MATERIALES

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$$\sigma = E \epsilon$$



$$\sigma = \eta \dot{\epsilon}$$

$$\begin{aligned} \sigma &= \eta \dot{\epsilon} \\ \Rightarrow \dot{\epsilon} &= \frac{\sigma}{\eta} \Rightarrow \epsilon(t) = \int_0^t \frac{\sigma}{\eta} dt \end{aligned}$$

Modelo de Maxwell



$\left. \begin{matrix} E \\ \eta \end{matrix} \right\}$ datos del material

En el modelo de Maxwell:

$$\sigma = \sigma(\epsilon) = \sigma(\eta)$$

La deformación es:

$$\epsilon = \epsilon^e + \epsilon^v \quad (A)$$

$$\sigma = E \epsilon^e \Rightarrow \epsilon^e = \frac{\sigma}{E} \rightarrow \text{Luego: } \dot{\epsilon}^e = \frac{\dot{\sigma}}{E} \quad (B)$$

$$\sigma = \eta \dot{\epsilon}^v \Rightarrow \dot{\epsilon}^v = \frac{\sigma}{\eta} \quad (C)$$

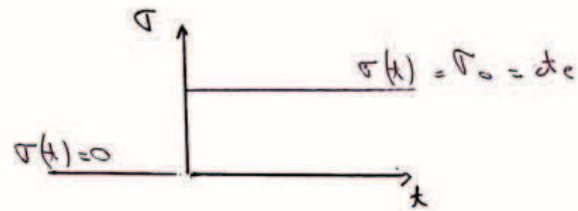
(B) y (C) \rightarrow (A):

$$\dot{\epsilon} = \dot{\epsilon}^e + \dot{\epsilon}^v$$

$$\Rightarrow \dot{\epsilon} = \frac{\dot{\sigma}}{E} + \frac{\sigma}{\eta} \quad (A')$$

- 2) Ensayo de creep

$$\boxed{\sigma(t) = \sigma_0} \quad t > 0$$



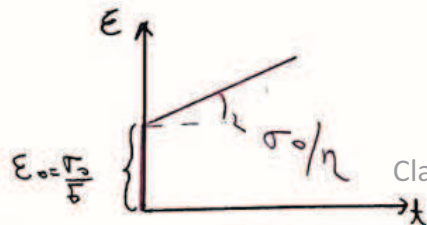
De la E.D.

$$\dot{\epsilon} = \frac{\dot{\sigma}}{E} + \frac{\sigma}{\eta}$$

$$\begin{aligned} \frac{d\epsilon}{dt} &= \frac{d\epsilon^e}{dt} + \frac{d\epsilon^v}{dt} \Rightarrow d\epsilon = \left(\frac{d\epsilon^e}{dt} + \frac{d\epsilon^v}{dt} \right) dt \\ &\Rightarrow \int d\epsilon = \int \frac{d\sigma^e}{dt} dt + \int \frac{\sigma}{\eta} dt \\ &\Rightarrow \epsilon(t) = \frac{\sigma}{E} + \int \frac{\sigma}{\eta} dt \end{aligned}$$

$$\Rightarrow \epsilon(t) = \frac{\sigma_0}{E} + \int_0^t \frac{\sigma_0}{\eta} dt (1)$$

$$\begin{aligned} \Rightarrow \boxed{\epsilon(t) = \frac{\sigma_0}{E} + \left(\frac{\sigma_0}{\eta} t \right)} \\ = \epsilon_0 + \frac{\sigma_0}{\eta} t \end{aligned}$$



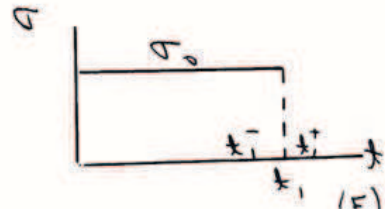
Lo (D) podemos expresarlo alternativamente en f.c. del t_p característico:

$$\tau = \eta/E \Rightarrow \frac{1}{\tau} = \frac{E}{\eta}$$

$$(E) \rightarrow \frac{\sigma_0}{E} + \frac{\sigma_0}{\eta} t = \frac{\sigma_0}{E} \left(1 + \frac{E}{\eta} t \right) \stackrel{\downarrow}{=} \frac{\sigma_0}{E} \left(1 + \frac{t}{\tau} \right) = \epsilon_0 + \epsilon_2 \frac{t}{\tau}$$

• Hemos tratado el creep. ¿Qué pasaría para un estado de carga más general? Veamos un ejemplo: una descarga instantánea para un $k = k_1$:

$$\sigma(t) = -\sigma_0 = 0 \quad k = k_1$$



Solo para $t > t_1^+$ $\sigma = 0$

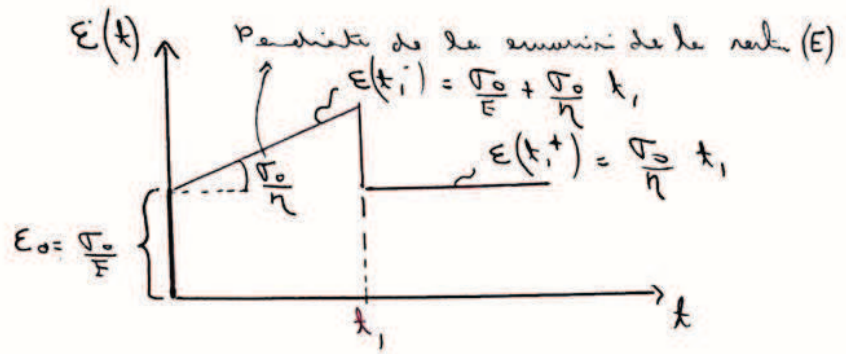
$$t = t_1^- \rightarrow \epsilon(t) = \frac{\sigma_0}{E} + \frac{\sigma_0}{\eta} t_1$$

$$t = t_1^+ \rightarrow \sigma_0 = 0 \rightarrow \epsilon(t_1^+) = \epsilon(t_1^-) - \left(\frac{\sigma_0}{E} + \int_{t_1^-}^{t_1^+} \frac{\sigma_0}{\eta} dt \right)$$

Eladio Carregio

$$= \frac{\sigma_0}{E} + \frac{\sigma_0}{\eta} t_1 - \frac{\sigma_0}{E}$$

$$\Rightarrow \boxed{\varepsilon(t_1^+) = \frac{\sigma_0}{\eta} t_1}$$



• Nota: \exists dos magnitudes que se suelen calcular para el problema viscoelástico:

$$\varepsilon(t) = J(t) \sigma_0 \quad \rightarrow \quad \text{De deformación: } J(t) = \frac{\varepsilon(t)}{\sigma_0}$$

$$\sigma(t) = E(t) \varepsilon_0 \quad \rightarrow \quad \text{De relajación: } E(t) = \frac{\sigma(t)}{\varepsilon_0}$$

$J(t)$: función de fluencia

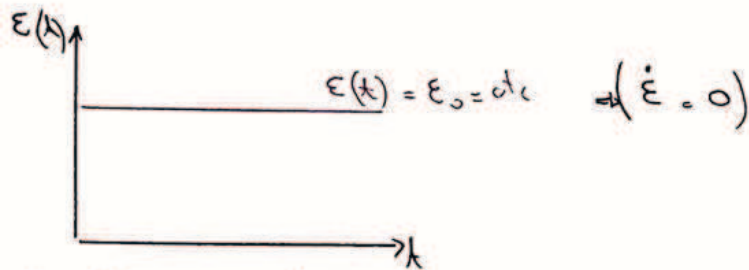
$E(t)$: módulo de relajación

Para el modelo de Maxwell del resultado del ensayo de creep resulta:

$$J(t) = \frac{1}{E} + \frac{t}{\eta}$$

- b) Ensayo de relajación (o de deformación etc)

$$\epsilon(t) = \epsilon_0 = \text{cte}$$



La E.D. de (A) :

$$\dot{\epsilon} = \frac{\dot{\sigma}}{E} + \frac{\sigma}{\eta}$$

$$\Rightarrow 0 = \frac{\dot{\sigma}}{E} + \frac{\sigma}{\eta}$$

$$\Rightarrow \frac{\dot{\sigma}}{E} = -\frac{\sigma}{\eta}$$

$$\Rightarrow \left(\frac{d\sigma}{\sigma} \right) = -\left(\frac{E}{\eta} \right) dt$$

$$\Rightarrow \ln \sigma = -\frac{E}{\eta} t + \text{cte}$$

$$\Rightarrow \sigma = e^{-\frac{E}{\eta} t + \text{cte}}$$

$$= e^{-\frac{E}{\eta} t} \underbrace{e^{\text{cte}}}_{\text{cte de A}}$$

$$= A e^{-\frac{E}{\eta} t} \quad (F)$$

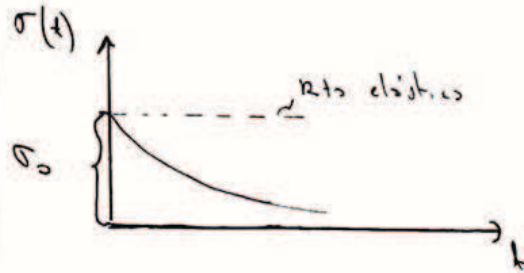
$$t=0 \rightarrow \sigma = A e^0 = A$$

$$\text{Pero: } \sigma = E \epsilon_0 \quad \text{en } t=0$$

$$\Rightarrow \text{Igualando: } A = E \epsilon_0 \quad (G)$$

$$\Rightarrow (G) \rightarrow (F):$$

$$\sigma = E \epsilon_0 e^{-\frac{E}{\eta} t} \quad (4)$$
$$= \sigma_0 e^{-\frac{E}{\eta} t}$$



- c) Ensayo con Velocidad de deformación cte

$$\dot{\epsilon} = cte = c$$

De E.D. (A'):

$$\begin{aligned}\dot{\epsilon} &= \frac{\dot{\sigma}}{E} + \frac{\sigma}{\eta} \\ &= c\end{aligned}\quad (I)$$

$$(I) \rightarrow \frac{\dot{\sigma}}{E} + \frac{\sigma}{\eta} = 0$$

$$\Rightarrow \frac{d\sigma}{dx} \frac{1}{E} = -\frac{\sigma}{\eta}$$

$$\Rightarrow \int \frac{d\sigma}{\sigma} = \int -\frac{E}{\eta} dx$$

$$\Rightarrow \ln \sigma = -\frac{E}{\eta} x + cte$$

$$\Rightarrow \sigma = e^{\left(-\frac{E}{\eta} x + cte\right)} = e^{-\frac{E}{\eta} x} e^{cte} = A e^{-\frac{E}{\eta} x} \quad (3)$$

• Solución particular:

$$\frac{\sigma}{\eta} = c = \dot{\epsilon}$$

$$\Rightarrow \frac{\sigma}{\eta} = \dot{\epsilon}$$

$$\Rightarrow \sigma = \eta \dot{\epsilon} \quad (K)$$

• Solución general:

$$\sigma(x) = A e^{-\frac{E}{\eta} x} + \eta \dot{\epsilon} \quad (L)$$

$$\text{Por } t=0 \rightarrow \sigma(t=0) = 0:$$

$$\rightarrow (L): 0 = A e^0 + \eta \dot{\epsilon}$$

$$\Rightarrow A = -\eta \dot{\epsilon} \quad (M)$$

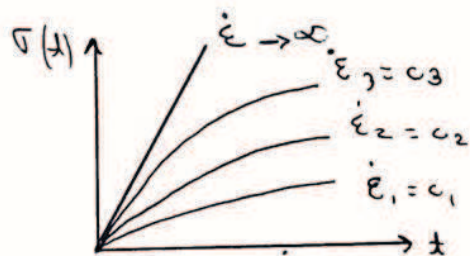
Luego $(M) \rightarrow L:$

$$\boxed{\sigma(t) = -\eta \dot{\epsilon} e^{-\frac{E}{\eta} t} + \eta \dot{\epsilon}} \quad (O)$$

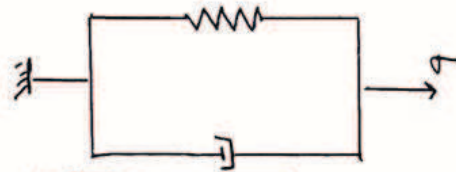
$$= \eta \dot{\epsilon} \left(1 - e^{-\frac{E}{\eta} t} \right) \quad (O')$$

\Downarrow

Se obtiene curvas de σ vs t para $t=0$ y $\sigma=0:$



Modelo de Kelvin-Voigt



$$\epsilon^e = \epsilon^v = \epsilon$$

$$\sigma_{\text{el}} = E \epsilon^e = E \epsilon$$

$$\sigma_{\text{visc}} = \eta \dot{\epsilon}^v = \eta \dot{\epsilon}$$

$$\sigma = \sigma_{\text{resorte}} + \sigma_{\text{amortiguador}}$$

$$\Rightarrow \sigma = E \epsilon + \eta \dot{\epsilon}$$

De esta última se podría obtener la E.D.

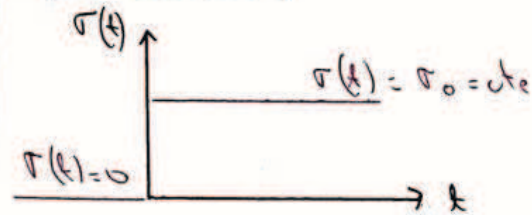
$$\Rightarrow \sigma - E \epsilon = \eta \dot{\epsilon}$$

$$\Rightarrow \frac{\sigma}{\eta} - \frac{E}{\eta} \epsilon = \dot{\epsilon}$$

$$\Rightarrow \dot{\epsilon} + \frac{E}{\eta} \epsilon = \frac{\sigma}{\eta} \quad \begin{matrix} (N) \\ (E.D.) \end{matrix}$$

2) Ensayo de creep

$$\sigma(t) = \sigma_0 \quad t > 0$$



De la E.D.:

$$\dot{\epsilon} + \frac{E}{\eta} \epsilon = \frac{\sigma_0}{\eta} \quad (P)$$

• Solución homogénea:

$$(P) \rightarrow \frac{d\epsilon}{dt} + \frac{E}{\eta} \epsilon = 0$$

$$\Rightarrow \frac{d\epsilon}{dt} = -\frac{E}{\eta} \epsilon$$

$$\Rightarrow \int \frac{d\epsilon}{\epsilon} = \int -\frac{E}{\eta} dt$$

$$\Rightarrow \ln \epsilon = -\frac{E}{\eta} t + cte$$

$$\Rightarrow \epsilon = e^{\left(-\frac{E}{\eta} t + cte\right)}$$
$$= e^{-\frac{E}{\eta} t} \underbrace{e^{cte}}_{=A}$$

$$\Rightarrow \epsilon = A e^{-\frac{E}{\eta} t}$$

(Q)

• Solución particular:

$$(P) \rightarrow \dot{\epsilon} + \frac{E}{\eta} \epsilon = \frac{\sigma_0}{\eta}$$

$$\Rightarrow \mathcal{E} = \frac{\sigma_0}{\kappa} \frac{\kappa}{E} \quad (R)$$

• Solución gen.:

Dc (Q) y (R):

$$\mathcal{E} = A e^{-\frac{E}{\eta} t} + \frac{\sigma_0}{E} \quad (S)$$

para $t=0 \rightarrow \mathcal{E}(t=0) = 0$

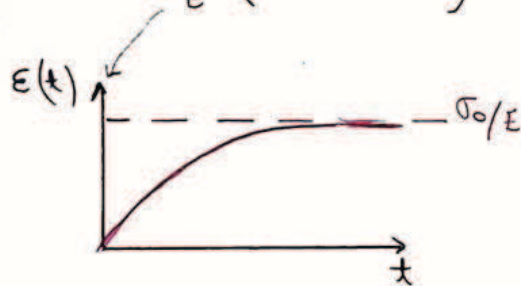
$$\Rightarrow 0 = A e^0 + \frac{\sigma_0}{E}$$

$$\Rightarrow A = -\frac{\sigma_0}{E} \quad (T)$$

Luego (T) \rightarrow (S):

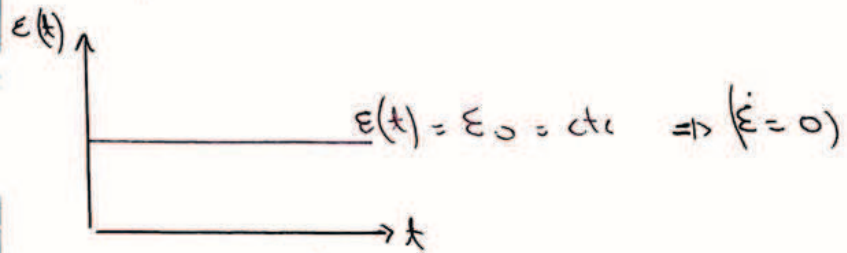
$$\mathcal{E}(t) = -\frac{\sigma_0}{E} e^{-\frac{E}{\eta} t} + \frac{\sigma_0}{E}$$

$$= \frac{\sigma_0}{E} \left(1 - e^{-\frac{E}{\eta} t} \right)$$



b) Ensayo de relajación:

$$\varepsilon(t) = \varepsilon_0 = \text{cte}$$



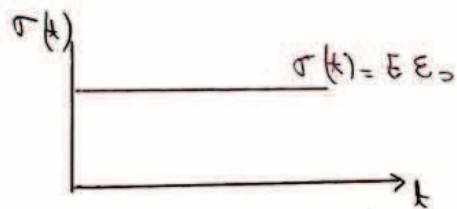
↳ E.D. de (N):

$$\dot{\varepsilon} + \frac{E}{\eta} \varepsilon = \frac{\sigma(t)}{\eta}$$

$$\Rightarrow \frac{E}{\eta} \varepsilon_0 = \frac{\sigma(t)}{\eta}$$

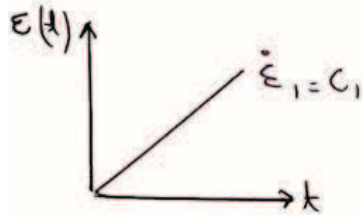
$$\Rightarrow \sigma(t) = \cancel{\eta} \frac{E}{\cancel{\eta}} \varepsilon_0 \quad \text{cte}$$

$$\Rightarrow \boxed{\sigma(t) = E \varepsilon_0} \\ = \text{cte}$$



c) Ensayo con velocidad de deformación cte:

$$\dot{\epsilon} = cte = c$$



De E.D. (U):

$$\dot{\epsilon} + \frac{E}{\eta} \epsilon = \frac{\sigma}{\eta}$$

$$\begin{aligned} \Rightarrow \sigma &= \eta \dot{\epsilon} + \eta \frac{E}{\eta} \epsilon \\ &= \eta \dot{\epsilon} + E \epsilon \end{aligned} \quad (U)$$

Luego

$$\dot{\epsilon} \equiv \frac{d\epsilon}{dt} \cong \frac{\epsilon}{t}$$

$$\Rightarrow \epsilon = \dot{\epsilon} t \quad (V)$$

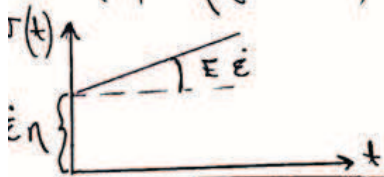
De (V) \rightarrow (U):

$$\sigma = \eta \dot{\epsilon} + E \dot{\epsilon} t$$

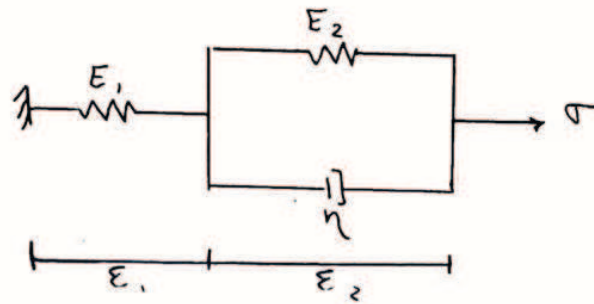
$$\Rightarrow \boxed{\sigma = \dot{\epsilon} (\eta + E t)} \quad (X)$$

• Para $t=0$, considerando (X):

$$\sigma(t=0) = \dot{\epsilon} (\eta + E \cdot 0) = \dot{\epsilon} \eta$$



Sólido lineal estándar:



Cinemáticos:

$$\epsilon = \epsilon_1 + \epsilon_2 \quad (1)$$

$$\dot{\epsilon} = \dot{\epsilon}_1 + \dot{\epsilon}_2 \quad (2)$$

De ecuación constitutiva del resorte:

$$\sigma = E_1 \epsilon_1 \quad (3)$$

con lo que:

$$\dot{\sigma} = E_1 \dot{\epsilon}_1 \quad (4)$$

De la E.D. del modelo de Kelvin-V.:

$$\begin{aligned} (4) \rightarrow \dot{\epsilon} + \frac{E}{\eta} \epsilon &= \frac{\sigma}{\eta} \\ \Rightarrow \sigma &= E_2 \epsilon_2 + \eta \dot{\epsilon}_2 \quad (5) \end{aligned}$$

Luego de (5):

$$\epsilon_2 = \frac{1}{E_2} (\sigma - \eta \dot{\epsilon}_2) \quad (6)$$

De (3) y (6) \rightarrow (1):

$$\epsilon = \frac{\sigma}{E_1} + \frac{1}{E_2} (\sigma - \eta \dot{\epsilon}_2) \quad (7)$$

De (2) \rightarrow (7):

$$\epsilon = \frac{\sigma}{E_1} + \frac{1}{E_2} [\sigma - \eta (\dot{\epsilon} - \dot{\epsilon}_1)] \quad (8)$$

De (4) \rightarrow (8):

$$\epsilon = \frac{\sigma}{E_1} + \frac{1}{E_2} \left[\sigma - \eta \left(\dot{\epsilon} - \frac{\dot{\sigma}}{E_1} \right) \right] \quad (9)$$

$$\Rightarrow \epsilon = \frac{\sigma}{E_1} + \frac{1}{E_2} \sigma - \frac{1}{E_2} \eta \dot{\epsilon} + \frac{\eta}{E_2} \frac{\dot{\sigma}}{E_1} \quad (10)$$

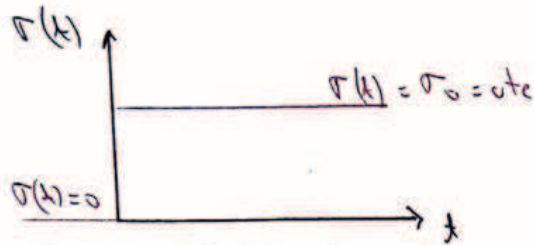
$$\Rightarrow \frac{1}{E_2} \eta \dot{\epsilon} + \epsilon = \frac{\eta}{E_1 E_2} \dot{\sigma} + \frac{E_1 + E_2}{E_1 E_2} \sigma \quad (11)$$

$$\Rightarrow \frac{\sigma, E_2}{\eta} \frac{\eta}{E_2} \dot{\epsilon} + \frac{E_1 E_2}{\eta} \epsilon = \dot{\sigma} + \frac{E_1 + E_2}{\eta} \sigma \quad (12)$$

$$\Rightarrow \boxed{E_1 \dot{\epsilon} + \frac{E_1 E_2}{\eta} \epsilon = \dot{\sigma} + \frac{E_1 + E_2}{\eta} \sigma} \quad (13) \text{ E.D.}$$

a) Ensayo de creep:

$$\boxed{\sigma(t) = \sigma_0} \quad t > 0 \quad (14)$$



Como $\sigma = \sigma_0 = cte$ entonces:
 $\dot{\sigma} = 0$ (15)

De (14) / (15) \rightarrow (13):

$$E_1 \dot{\epsilon} + \frac{E_1 E_2}{\eta} \epsilon = \frac{E_1 + E_2}{\eta} \sigma_0 \quad (16)$$

• Solución homogénea:

$$(16) \rightarrow \widehat{E}_1 \dot{\epsilon} + \frac{\widehat{E}_1 E_2}{\eta} \epsilon = 0 \quad (17)$$

$$\Rightarrow \dot{\epsilon} + \frac{E_2}{\eta} \epsilon = 0 \quad (18)$$

$$\Rightarrow \frac{d\epsilon}{dt} = -\frac{E_2}{\eta} \epsilon \quad (19)$$

$$\Rightarrow \frac{d\epsilon}{\epsilon} = \left(-\frac{E_2}{\eta} dt \right) \quad (20)$$

$$\Rightarrow \ln \epsilon = -\frac{E_2}{\eta} t + cte \quad (21)$$

$$\Rightarrow \epsilon = e^{(-\frac{E_2}{\eta} t + cte)} = e^{-\frac{E_2}{\eta} t} e^{cte} \quad (22)$$

$$\Rightarrow \epsilon = A e^{-\frac{E_2}{\eta} t} \quad (23)$$

Audio Careglio

• Solución particular

$$(16) \rightarrow \cancel{E_1} \cancel{E} + \frac{E_1 E_2}{\lambda} E = \frac{E_1 + E_2}{\lambda} \sigma_0 \quad (24)$$

$$\Rightarrow E = \frac{\cancel{\lambda}}{E_1 E_2} \frac{E_1 + E_2}{\cancel{\lambda}} \sigma_0 \quad (25)$$

• Solución gen: σ_0 :

De (23) y (25):

$$E(t) = A e^{-\frac{E_2}{\lambda} t} + \frac{E_1 + E_2}{E_1 E_2} \sigma_0 \quad (26)$$

Para $t=0$:

$$(3) \rightarrow E_0 = \frac{\sigma_0}{E_1} \quad (27)$$

$$\Rightarrow (27) \rightarrow (26): \frac{\sigma_0}{E_1} = A \underbrace{e^{-\frac{E_2}{\lambda} t=0}}_{=1} + \frac{E_1 + E_2}{E_1 E_2} \sigma_0 \quad (28)$$

$$\Rightarrow A = \frac{\sigma_0}{E_1} - \frac{E_1 + E_2}{E_1 E_2} \sigma_0 \quad (29)$$

$$= \sigma_0 \left(\frac{1}{E_1} - \frac{E_1 + E_2}{E_1 E_2} \right) = \frac{\sigma_0}{E_1} \left(1 - \frac{E_1 + E_2}{E_2} \right) \quad (30)$$

$$= \frac{\sigma_0}{E_1} \left(\frac{\cancel{E_2} - E_1 - \cancel{E_2}}{E_2} \right) = \frac{\sigma_0}{\cancel{E_1}} \left(-\frac{E_1}{E_2} \right) \quad (31)$$

$$= -\frac{\sigma_0}{E_2} \quad (32)$$

Luego:

$$(32) \rightarrow (26): E(t) = -\frac{\sigma_0}{E_2} e^{-\frac{E_2}{\lambda} t} + \frac{E_1 + E_2}{E_1 E_2} \sigma_0 \quad (33)$$

$$\Rightarrow \boxed{\varepsilon(x) = \frac{\sigma_0}{E_2} \left(\frac{E_1 + E_2}{E_1} - e^{-\frac{E_2}{\lambda} x} \right)} \quad (34)$$

- vamos agora graficamente como es de $\varepsilon(x)$:

• Para $x \rightarrow \infty$:

$$(34) \rightarrow : \varepsilon(x \rightarrow \infty) = \frac{\sigma_0}{E_2} \frac{E_1 + E_2}{E_1} \quad (35)$$

$$= \frac{\sigma_0}{\left(\frac{E_1 E_2}{E_1 + E_2} \right)} \quad (36)$$

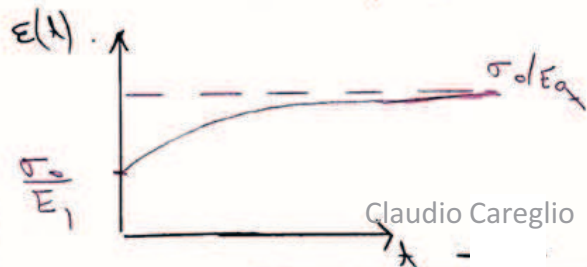
$$= \frac{\sigma_0}{E_p} \quad (37)$$

• Para $x = 0$:

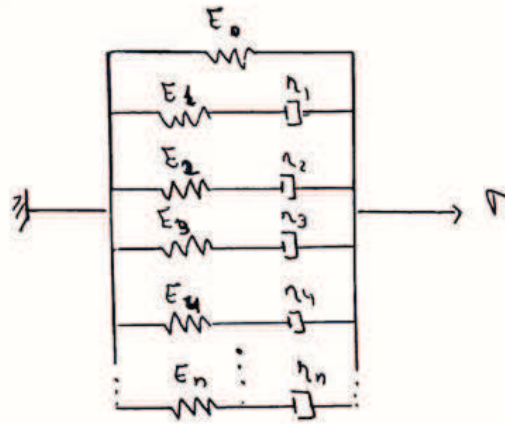
$$(34) \rightarrow \varepsilon(x=0) = \frac{\sigma_0}{E_2} \left(\frac{E_1 + E_2}{E_1} - e^0 \right) \quad (38)$$

$$= \frac{\sigma_0}{E_2} \frac{E_2}{E_1} = \frac{\sigma_0}{E_1} \quad (39)$$

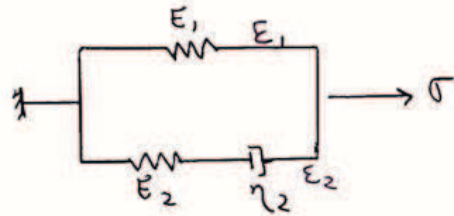
• Por lo que el gráfico de $\varepsilon(x)$:



Modelo de Maxwell generalizado



Para nuestro análisis consideremos como ejemplo un modelo de Maxwell generalizado de 1 ramo.



Cinemática:

$$\epsilon = \epsilon_1 = \epsilon_2 \quad [1]$$

Por equilibrio:

$$\sigma = \sigma_1 + \sigma_2 \quad [2]$$

$$\Rightarrow \dot{\sigma} = \dot{\sigma}_1 + \dot{\sigma}_2 \quad [3]$$

De ecuación constitutiva del resorte en la rama 1:

$$\sigma_1 = E_1 \epsilon \quad [4]$$

$$\Leftrightarrow \epsilon = \frac{\sigma_1}{E_1}$$

$$\Rightarrow \dot{\sigma}_1 = E_1 \dot{\epsilon} \quad [5]$$

En la rama del modelo de Maxwell:

$$\varepsilon_2 = \varepsilon_2 \text{ amortiguador} + \varepsilon_2 \text{ resorte} \quad [7]$$

$$\downarrow [1] \\ = \dot{\varepsilon} \quad [8]$$

$$\Rightarrow \dot{\varepsilon}_2 = \dot{\varepsilon} \quad [9]$$

$$= \dot{\varepsilon}_2 \text{ amort.} + \dot{\varepsilon}_2 \text{ resorte} \quad [10]$$

$$\sigma_2 \text{ resor.} = E_2 \varepsilon_2 \text{ resor.} \quad [11]$$

$$= \sigma_2 \quad [12]$$

$$\Rightarrow \dot{\varepsilon}_2 \text{ res.} = \frac{\dot{\sigma}_2}{E_2} \quad [13]$$

$$\sigma_2 \text{ amort.} = \eta_2 \dot{\varepsilon}_2 \text{ amort.} \quad [14]$$

$$= \sigma_2 \quad [15]$$

$$\Rightarrow \dot{\varepsilon}_2 \text{ amort.} = \frac{\sigma_2}{\eta_2} \quad [16]$$

De [13] y [16] \rightarrow [10]:

$$\dot{\varepsilon}_2 = \dot{\varepsilon} = \frac{\sigma_2}{\eta_2} + \frac{\dot{\sigma}_2}{E_2} \quad [17]$$

$$\Rightarrow \dot{\varepsilon} - \frac{\sigma_2}{\eta_2} = \frac{\dot{\sigma}_2}{E_2} \quad [18]$$

$$\Rightarrow \dot{\sigma}_2 = E_2 \left(\dot{\varepsilon} - \frac{\sigma_2}{\eta_2} \right) \quad [19]$$

De [6] y [19] \rightarrow [3]:

$$\dot{\sigma} = E_1 \dot{\varepsilon} + E_2 \left(\dot{\varepsilon} - \frac{\sigma_2}{\eta_2} \right) \quad [20]$$

$$= E_1 \dot{\varepsilon} + E_2 \dot{\varepsilon} - \frac{E_2 \sigma_2}{\eta_2} \quad [21]$$

pero:

$$[2] \rightarrow \sigma_2 = \sigma - \sigma_1$$

$$= \sigma - E_1 \epsilon$$

[22]

[23]

[23] \rightarrow [21]:

$$\dot{\sigma} = E_1 \dot{\epsilon} + E_2 \dot{\epsilon} - \frac{E_2}{\eta_2} (\sigma - E_1 \epsilon)$$

[24]

$$= (E_1 + E_2) \dot{\epsilon} - \frac{E_2}{\eta_2} \sigma + \frac{E_2 E_1}{\eta_2} \epsilon$$

[25]

$$\Rightarrow \boxed{\dot{\sigma} + \frac{E_2}{\eta_2} \sigma = \frac{E_2 E_1}{\eta_2} \epsilon + (E_1 + E_2) \dot{\epsilon}}$$

E.O. [26]

lo que puede reescribirse:

$$\dot{\sigma} + p_0 \sigma = q_0 \epsilon + q_1 \dot{\epsilon}$$

$$= \frac{E_2}{\eta_2} \epsilon = \frac{E_1 E_2}{\eta_2} \epsilon = (E_1 + E_2) \dot{\epsilon}$$

p_0, q_0, q_1 : coef. caracter.

En la ecuación [26] se puede utilizar para analizar creep, relajación, etc.

a) Ensayo de creep: (Ejercicios para alumnos)

b) Ensayo de relajación: (Ejercicios para alumnos)

Comportamiento en equilibrio:

Dado que Maxwell generalizado suele usarse en la práctica es que se analiza más en detalle.

Con este fin se estudia el comportamiento en equilibrio y en transitorio (no equilibrio).

Después un tiempo grande $t \rightarrow \infty$ se alcanza un estado de equilibrio y el modelo realístico debe estar en reposo. En este caso:

$$\dot{\xi} = 0$$

$$\Rightarrow \sigma_{\text{trans.}} = 0$$

por equilibrio resulta:

$$\sigma_{\text{resorte}} = 0$$

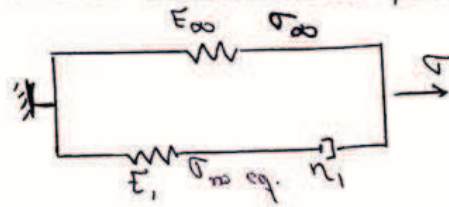
$$\sigma = \underbrace{\sigma_{\infty}} + \underbrace{\sigma_{n. eq.}}$$

Tensión en
la rama con
resorte solo

↓
y el módulo de
Young se lo llama
 E_{∞}

Tensión que corresponde a un estado de
no equilibrio (tiene lugar en que de
las ramas de Maxwell)

Planteo termodinámico y variables internas



Cinemáticas:

$$\varepsilon = \varepsilon_1$$

$$\varepsilon_1 = \varepsilon_1^e + \varepsilon_1^v$$

$$\Rightarrow \dot{\varepsilon}_1 = \dot{\varepsilon}_1^e + \dot{\varepsilon}_1^v$$

Por equilibrio:

$$\sigma = \sigma_\infty + \sigma_{no eq.} \quad [A]$$

De ecuación constitutiva:

$$\sigma_\infty = E_\infty \varepsilon \quad [B]$$

$$\begin{aligned} \sigma_{no eq.} &= E_1 \varepsilon_1^e \\ &= E_1 (\varepsilon - \varepsilon_1^v) \end{aligned}$$

$$= \eta_1 \dot{\varepsilon}_1^v \quad [C]$$

Se puede obtener una ecuación de la cual se obtenga la evolución de ε_1^v

$$\dot{\varepsilon}_1^v = \frac{E_1}{\eta_1} (\varepsilon - \varepsilon_1) = \frac{1}{\tau} (\varepsilon - \varepsilon_1)$$

Partiendo de las expresiones de la energía libre (asumiendo formas cuadráticas para ambos resortes):

$$\Psi = \Psi_{\infty} + \Psi_{\text{no eq.}}$$

$$= \underbrace{\frac{1}{2} \varepsilon E_{\infty} \varepsilon}_{\boxed{E}} + \underbrace{\frac{1}{2} (E - E_1^v) E_1 (E - E_1^v)}_{\boxed{F}} \quad \boxed{D}$$

Luego:

$$\dot{\Psi} = \dot{\Psi}_{\infty} + \dot{\Psi}_{\text{no eq.}}$$

$$= \frac{\partial \Psi_{\infty}}{\partial E} \dot{E} + \frac{\partial \Psi_{\text{no eq.}}}{\partial (E - E_1^v)} (\dot{E} - \dot{E}_1^v)$$

Considerando la desigualdad de Clausius:

$$-\dot{\Psi} + \sigma : \dot{E} \geq 0$$

$$\Rightarrow - \left(\frac{\partial \Psi_{\infty}}{\partial E} \dot{E} + \frac{\partial \Psi_{\text{no eq.}}}{\partial (E - E_1^v)} (\dot{E} - \dot{E}_1^v) \right) + \sigma : \dot{E} \geq 0$$

$$\Rightarrow - \frac{\partial \Psi_{\infty}}{\partial E} \dot{E} - \frac{\partial \Psi_{\text{no eq.}}}{\partial (E - E_1^v)} \dot{E} + \frac{\partial \Psi_{\text{no eq.}}}{\partial (E - E_1^v)} \dot{E}_1^v + \sigma : \dot{E} \geq 0$$

Reagrupando términos:

$$\left(\frac{\partial \Psi_{\infty}}{\partial E} \sigma + \sigma \right) \dot{E} + \left(- \frac{\partial \Psi_{\text{no eq.}}}{\partial (E - E_1^v)} + \sigma_{\text{no eq.}} \right) \dot{E} + \frac{\partial \Psi_{\text{no eq.}}}{\partial (E - E_1^v)} \dot{E}_1^v \geq 0$$

Analizando ahora el término:

$$\sigma_{\infty} = \frac{\partial \Psi_{\infty}}{\partial E}$$

$$\stackrel{\boxed{E}}{\Downarrow} \frac{\partial}{\partial E} \left[\frac{1}{2} \varepsilon E_{\infty} \varepsilon \right]$$

$$= E_{\infty} \varepsilon$$

$$\begin{aligned}
 \sigma_{no\ eq.} &= \frac{\partial \psi_{no\ eq.}}{\partial (\varepsilon - \varepsilon_1^v)} \\
 &\stackrel{\text{E}}{=} \frac{\partial}{\partial (\varepsilon - \varepsilon_1^v)} \left[\frac{1}{2} (\varepsilon - \varepsilon_1^v) \varepsilon_1 (\varepsilon - \varepsilon_1^v) \right] \\
 &\stackrel{\text{C}}{=} \varepsilon_1 (\varepsilon - \varepsilon_1^v) \quad \text{G} \\
 &\stackrel{\text{H}}{=} \eta_1 \dot{\varepsilon}_1^v \quad \text{H}
 \end{aligned}$$

$$\begin{aligned}
 D &= \frac{\partial \psi_{no\ eq.}}{\partial (\varepsilon - \varepsilon_1^v)} \dot{\varepsilon}_1^v > 0 \\
 \Rightarrow D &\stackrel{\text{G}}{=} \varepsilon_1 (\varepsilon - \varepsilon_1^v) \dot{\varepsilon}_1^v \quad \text{I} \\
 &\stackrel{\text{H}}{=} \eta_1 \dot{\varepsilon}_1^v \varepsilon_1^v \\
 \Rightarrow D &= \eta_1 \dot{\varepsilon}_1^v{}^2 > 0 \quad \text{J}
 \end{aligned}$$

$D < 0$:
 $\varepsilon_1 (\varepsilon - \varepsilon_1^v) \dot{\varepsilon}_1^v = \eta_1 \dot{\varepsilon}_1^v \neq$

$$\Rightarrow \dot{\varepsilon}_1^v = \frac{\varepsilon_1 (\varepsilon - \varepsilon_1)}{\eta_1} = \frac{1}{2} (\varepsilon - \varepsilon_1)$$

Set of
 exclusion
 K

$$p = - \frac{\partial \psi}{\partial \dot{\epsilon}_1^v}$$

$$\begin{aligned} \Rightarrow p &\stackrel{\boxed{D}}{=} - \frac{\partial}{\partial \dot{\epsilon}_1^v} \left[\frac{1}{2} \epsilon \epsilon_2 \epsilon + \frac{1}{2} (\epsilon - \epsilon_1^v) \epsilon_1 (\epsilon - \epsilon_1^v) \right] \\ &= - \left[(\epsilon - \epsilon_1^v) \epsilon_1 \right] \\ &= + \epsilon_1 (\epsilon - \epsilon_1^v) \quad \boxed{L} \end{aligned}$$

Combinando \boxed{L} con \boxed{B} :

$$p = \sigma \text{ no eq.}$$

Se puede verificar que:

$$\begin{aligned} D &= p \cdot \dot{\epsilon}_1^v = \epsilon_1 (\epsilon - \epsilon_1^v) \dot{\epsilon}_1^v \\ &= \eta_1 \dot{\epsilon}_1^v{}^2 \end{aligned}$$